# CHEMICAL MONITORING OF THE IN-SITU LEACHING OF A SOUTH TEXAS URANIUM OREBODY

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#### INTRODUCTION

In-situ leaching of orebodies is an extraction technology that has the potential of being an economical method of ore extraction as well as being the method that has the least adverse impact on the environment. Currently, large-scale extraction of uranium is being done economically by in-situ technology. To date, all large-scale in-situ leaching of uranium orebodies has been confined to southwest Texas; however, the imminent spread of this type mining to other states is indicated from pilot tests being conducted in other areas. Despite the successful application of in-situ leaching technology to the extraction of uranium, many features of the leaching process are not fully understood.

In order to elucidate the process of the in-situ leaching of uranium as well as to provide tests of various components used in in-situ leaching, the U.S. Bureau of Mines (USBM) initiated a cooperative monitoring test of a commercial in-situ leach operation in south Texas. The U.S. Geological Survey (USGS) was asked by the USBM to participate in the project in order to provide expertise in the geochemistry and mineralogy of the process. It was hoped that by augmenting the project with these types of data, information would be obtained that would aid in increasing recoveries and lessening any adverse impacts on the environment. This report is a summary of the data collected.

The geochemical and mineralogic data collection was broken down into two separate phases. The first phase, baseline data collection, consisted of establishing the initial conditions of the host rock and formation waters prior to the introduction of any lixiviant. This baseline characterization included the comprehensive mineralogy of the core samples obtained by the USBM from the leaching pattern and water analyses of the formation waters in the leaching pattern as well as from peripheral monitoring wells. The second phase involved the collection of comprehensive chemical data on the composition of the formation waters as a function of time during the leaching of the orebody. In addition to the geochemical and mineralogic data collected during these basic phases, performance data on field analytical methods, sampling and preservation methods, and on a downhole, gas-tight sampler were obtained. Such performance data are applicable for setting standards for the collection and analysis of samples, in order that standardized and meaningful chemical data may be obtained for purposes of requiring comparison, such as are involved in environmental questions.

#### BASELINE CHARACTERIZATION

# Mineralogy of the Host Formation

The USBM provided core samples of the host formation. These samples consisted of four sections of sandstone (USBM-2, USBM-4, USBM-7, and USBM-8) and one section of the upper shale unit (USBM-2a). General data for the four samples of uraniferous sands studied are reported in table 1. All weight percentages shown are proportions of the entire sample used (rather than proportions of a particular mesh size or gravity fraction) so that each entry may be directly compared and its importance to the overall sample assessed. Colors and sample weights were noted for the samples as received and when dry. Approximately 10 g of each sample was removed for reference and later checks. A whole-rock X-ray diffraction pattern was then made using about 0.7 g of each sample. Clay minerals were separated using distilled water and oriented slides were prepared for X-ray The decanted water was evaporated in order to identify the water-soluble minerals present. Examination of the carbonates in the core material both optically and by X-ray revealed them to be essentially CaCO, hence the calcite content was determined by leaching it from the samples with 1:10 HCl. The remaining sand fraction was size-sorted by sieving. The -40 +80 mesh fraction of each of the samples was further separated using heavy liquids. X-ray and optical studies were then carried out for each fraction and for some minerals handpicked for special study.

. Table 1. Data for samples of uraniferous sands from Texas

Sample number	USBM-2		USBM-4		USBM-7		USBM-8	
Color (damp)	pale oli 5Y 6/		olive gr 5Y 4/		light ol 5Y 5/	ive gray	medium o 5Y 5/	live gray l
Color (dry)	yellowis 5Y 7/	h-gray	pale oli 5Y 6/		pale oli 5Y 6/		pale oli 5Y 6/	
Sample Weight	070		106	•	107	•	164	•
(as rec'd; g)	270 254		196 186		187 178		152	
(dry; g)		.0 .7	_	.0		.8		.3
H <sub>2</sub> 0 (Weight %)	,	• /	,	• •	•	••0	,	
	Wt. (g)	Wt. 7	Wt. (g)	Wt. 7	Wt. (g)	Wt. Z	Wt. (g)	Wt. 7
Study sample	234.4		175.2		166.7		142.3	
Clay minerals	23.4	9.6	12.3	7.0	11.3	6.8	9.1	6.4
Water soluble	0.2	0.1	0.2	0.1	0.2	0.1	0.2	0.1
Calcite	33.8	13.9	15.7	9.0	18.7	11.2	13.0	9.1
Sand (all other)	186.0	76.4	147.0	83.9	136.5	81.9	120.0	84.3
Total	243.4	100.0	175.2	100.0	166.7	100.0	142.3	99.9
Sand (Mesh size)								
+20	0.0	0.0	0.1	<0.1	0.0	0.0	0.0	0.0
-20 +40	5.6	2.3	8.5	4.8	1.2	0.7	2.2	1.5
-40 +80	142.4	58.5	120.3	68.7	93.4	<b>56.</b> 0	105.3	74.0
-80 +120	25.1	10.3	11.0	6.3	21.7	13.0	5.9	4.1
-120	12.9	5.3	7.1	4.1	20.1	12.1	6.6	4.6
Total	186.0	76.4	147.0	83.9	136.4	81.8	120.0	84.2
Sand (-40 +80)								
Specific gravity								
<2.28	1.9	0.8	0.1	<0.1	0.1	<0.1	0.03	<0.1
2.28-2.57	46.0	18.9	12.1	6.9	13.7	8.2	4.2	3.0
2.57-2.62	63.2	26.0	11.1	6.3	15.8	9.5	16.3	11.4
2.62-2.67	27.2	11.2	93.2	53.2	58.5	35.1	82.4	57.9
2.67-2.85	2.7	1.1	2.8	1.6	4.4	2.6	1.6	1.1
2.85-3.31	1.4	0.5	0.7	0.4	0.4	0.2	0.4	0.3
> 3.31			0.3	0.2	0.4	0.2	0.4	0.3
Total	142.4	58.5	120.3	68.6	93.3	55.8	105.3	74.0

Table 1a. Mineralogy of uraniferous sands. Values in weight percent.

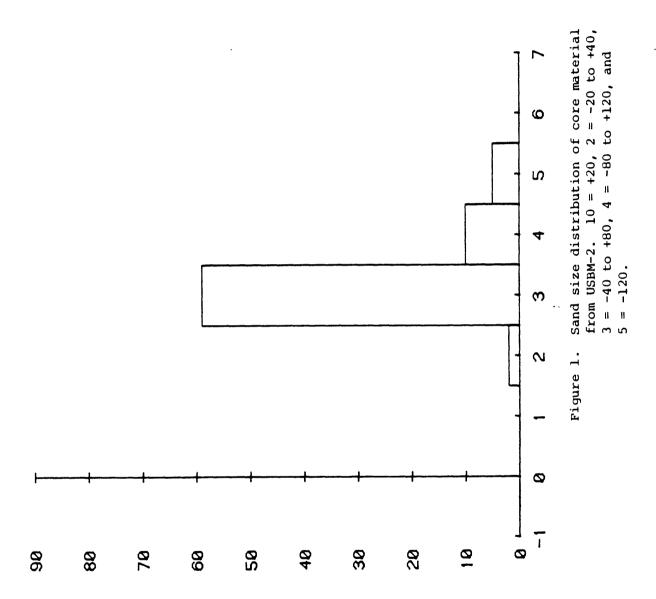
	USBM 2	USBM 4	USBM 7	USBM 8
Quartz	53	55	49	 59
K-feldspar	12	13	15	12
Plagioclase	11	12	16	12
Calcite	13.9	9.0	11.2	9.1
Clays	7.4	7.0	6.8	6.4
Pyrite	1.2	1.5	.4	.6
Clinoptilolite	2	2	1.5	1.0

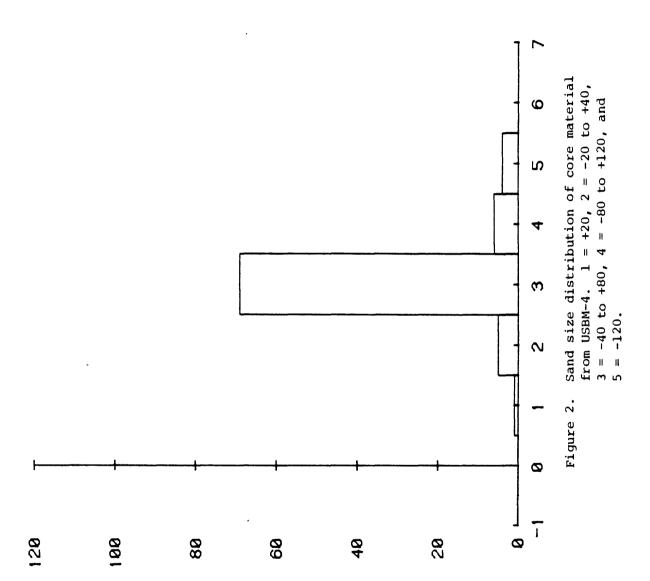
All of the four sand samples studied are similar to each other. Clay minerals are chiefly Ca-montmorillonite with subordinate, randomly-interstratified chlorite and illite. Calcite, quartz, pyrite, feldspars, and clinoptilolite are also present in minor amounts in the clay-size fraction. The water-soluble salts precipitated from the distilled-water leach were invariably found to be gypsum with minor calcite and halite. No gypsum was found in any of the sand samples, however. All of the water-soluble fractions gave positive tests for boron. Based on these observations it would appear that all of these materials were derived from the evaporation of formation water from the core material and do not represent solid phases actually present in the host formation. Calcite is present as a cementing matrix between the clastic grains, as coarse fragments of pyritiferous limestone and shell material, as finer grains of foraminifera, and as clay-size material. No aragonite or other carbonates were found.

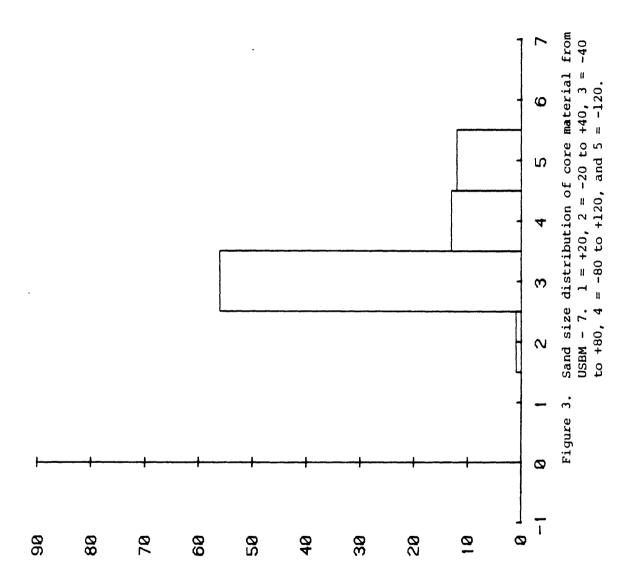
The <u>sand</u> fraction is composed chiefly of quartz (many varieties and types: see detailed sand descriptions), chert, K-feldspars (microcline and sanidine), plagioclase, iron sulfides, and very minor heavy minerals. Magnetic minerals are notably absent from all samples. The grains are loosely-cemented to well-cemented with pyrite and calcite. The proportion of attached pyrite makes a slight inaccuracy in the weight of the specific gravity fractions.

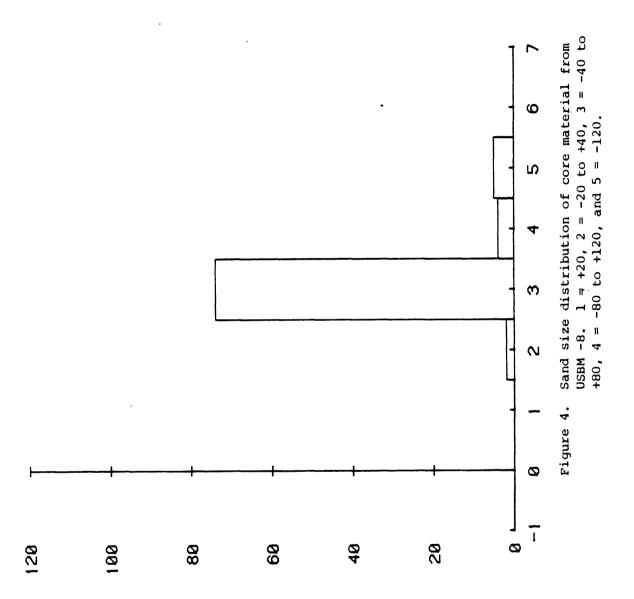
The size distribution (figs. 1, 2, 3, 4), heterogeneity of quartz grains, relative absence of heavy minerals, and fossil content suggest that these are samples of a beach sand. The K-feldspars are maximum microcline and subordinate sanidine; orthoclase and adularia are scarce to absent. The sanidine is vitreous and fresh with inclusions of biotite, whereas the microcline is mostly weathered and partially altered to clay minerals (montmorillonite). Plagioclase includes the ranges from  ${\rm An}_0$  to approximately  ${\rm An}_{45}$ ; more calcic material may be present, but was not detected in this study. Pyrite is more abundant in the coarser grain sizes with marcasite increasing in abundance in the finer fractions.

Pyrite is invariably the matrix material other than calcite cementing the clastic grains. Some of the clinoptilolite is black and nearly opaque from included pyrite, and some clinoptilolite grains appear to be pyrite pseudomorphs.









# Detailed Sand Franction Descriptions

#### USBM-2

- -20 +40 mesh. Has the same minerals, in general, as the -40 +80 mesh size (described below). Noteworthy are several subhedral to euhedral crystals of clinoptilolite colored black with inclusions of fine-grained pyrite.
- -40 +80 mesh. This fraction, which makes up almost 70% of the whole sample, was studied in more detail than the other size fractions. It was separated, with heavy liquids, into the following components having the indicated specific gravities:
  - >2.85. Mostly marcasite with minor pyrite. A very small, weakly magnetic, fraction consists of rounded ilmenite grains coated with pyrite. There is no magnetite present. Heavy minerals are virtually absent from the total sand sample as they constitute only about five percent of this fraction (or less than 0.05% of the whole sample). The heavy minerals, in approximate order of abundance, are sphene, zircon, tourmaline (schorl; dravite), garnet (not identified), and biotite.
  - 2.85 2.67. Mostly quartz and calcite with minor albite and very minor microcline.
- 2.67 2.62. Quartz, microcline, and albite. The quartz grains are predominantly angular to subangular, but some are well rounded. About one-third of the quartz present is in the form of chalcedony: mostly black and opaque, but some reddish brown and translucent. The feldspar is subangular and weathered.

2.62 - 2.57. Microcline, quartz, and very minor clinoptilolite. The microcline ranges from weathered to nearly fresh and from colorless, through white, to black from unidentified included material. Handpicked, fresh, colorless to white grains give an X-ray diffraction pattern of maximum microline:

These dimensions indicate a composition of  $0r_{96-98}$ .

2.57 - 2.28. Almost entirely microcline with minor quartz as determined by optical examination. The feldspar is mostly weathered.

<2.28. Microcline, minor quartz, and clinoptilolite. The microcline in this fraction is chiefly white and considerably attacked by weathering. A portion of the microcline has the form of rounded white nodules; the X-ray diffraction pattern of this microcline exhibits broad peaks with weak intensities. However, no clay minerals nor other alteration products could be detected in this material. There is also a smaller amount of gray microcline present.</p>

The clinoptilolite is present both as platy euhedral crystals, rosettes, and fine-grained massive material. The coarser crystals are black and nearly opaque from included pyrite. Designation as clinoptilolite is based on the thermal stability of the structure to temperatures up to 700°C in heating experiments. The clinoptilolite had the unit-cell dimensions:

<u>a</u> (Å)	17.70(1)
<u>b</u>	17.92(1)
<u>c</u>	7.416(3)
β	116° 23(3)'
V (A <sup>3</sup> )	2107(2)

\_80 +120 mesh. Separated into sp gr >2.85 (0.8 g; 2.5 wt.%) and sp gr <2.85 (31.2 g; 97.5 wt.%). The heavy fraction is composed of marcasite with subordinate pyrite. Heavy minerals are less than 5%. The light fraction is mostly quartz with calcite and minor microcline and albite.

-120 mesh. Separated into sp gr >2.85 (1.6 g; 7.6 wt.%) and sp gr <2.85 (19.4 g; 92.4 wt.%). Compositions of both fractions are similar to the -80 +120 mesh fractions above, but marcasite is relatively more abundant in the heavy fraction and calcite is more abundant in the light fraction in the finer mesh size.

#### USBM-4

-20 +40 mesh (whole fraction): Quartz, plagioclase, K-feldspar, pyrite, and clinoptilolite. Microcline is present as light gray nodules with inclusions of pyrite. About 15% of the total sand sample is composed of smoky quartz which is very dis-tinctive. It is most abundant in this mesh size and becomes scarcer as the mesh size decreases. It appears as subhedral crystals to angular fragments, is transparent, and colored light reddish brown. color disappears after heating to 300°C for several hours. Some of the angular fragments are 1.5 mm in greatest dimension, but the subhedral to euhedral crystals are as small as 0.45 mm in diameter so that there is a fair range in size. The smoky color has been attributed to free Si formed by natural irradiation. This may well have been the cause of the color of this smoky quartz at the original source, but it is unlikely in-situ as there is a great variety of associated quartz showing no such effects. The source of this quartz may be quite local, however, for there is very little evidence of rounding, abrasion, or other effects of transport. Smoky quartz is most abundant in this sample. There is less than ten percent in sample USBM-7 and only an occasional grain can be found in sample USBM-8.

- -4 +80 mesh. As shown in table 1, this fraction makes up nearly 70% of the whole sample. It was separated with heavy liquids into the various specific gravity fractions discussed below.
  - $\geq 3.31$ . Pyrite, clinoptilolite, and marcasite. There is more of the zeolite in this fraction than in the lighter fractions due to the included or replacing pyrite. Heavy minerals which are mostly yellow sphene, garnet, and zircon are present as minor constituents (less than ten percent of this fraction). 3.31-2.85. Quartz (with attached pyrite), plagioclase, K-feldspar, pyrite, clinoptilolite, marcasite, and micas. Less than two percent of this fraction is composed of white, frosted, prismatic grains of fluorapatite ( $\omega-1.634$ ). Minor heavy minerals: sphene, tourmaline, and garnet.
  - 2.85 2.67. Quartz, plagioclase, K-feldspar, minor pyrite, marcasite, and trace of muscovite. Much of the plagioclase is andesine (approximately An<sub>45</sub>) and occurs as prismatic to tabular subhedral clasts showing etching and other effects of solution. There are minor, but distinctive, green clasts of pyritiferous schist composed of quartz, plagioclase, green muscovite (chromiferous?), and chlorite.
  - 2.67 2.62. Constitutes over 50% of the whole sample. Quartz, K-feldspar, and plagioclase. There is a wide variety of quartz present. It varies from clear to opaque; colorless to black; coarsely crystalline to compact; fresh and angular to rounded and frosted. There is a major amount of deep brownish-black chert present.

2.62 - 2.57. K-feldspar (microcline, sanidine), plagioclase, quartz, and trace of pyrite. Some of the microcline in this fraction is nearly black; some is light gray with small spherules of pyrite. The microcline appears as block subangular to subrounded clasts. Sanidine is colorless, angular, subhedral, with some inclusions of biotite.

2.57 - 2.28. Microcline, quartz.

<2.28. Weatherered microcline with minor plagioclase, pyrite, and clinoptilolite.

-80 +120 mesh (whole fraction). Mostly quartz with subordinate
 K-feldspar, plagioclase, and very minor pyrite and muscovite.
 -120 mesh (whole fraction). Quartz with K feldspar and plagioclase.

#### USBM-7

This sample is closely similar in most respects to sample USBM-4 and, except for some details, only a generalized description is given here.

-20 +40 mesh (whole fraction). Quartz, plagioclase, K-feldspar, pyrite, and clinoptilolite.

#### -40 +80 mesh (specific gravity fractions).

>3.31. Pyrite, marcasite, and minor sphene, garnet, and trace of zircon. Heavy minerals are less than ten percent of this and the following fraction.

3.31 - 2.85. Pyrite, marcasite, quartz (with attached pyrite), clinoptilolite (with pyrite), and minor fluorapatite, sphene, tourmaline, and garnet.

- 2.85 2.67. Quartz, plagioclase, pyrite, and minor mica (chiefly muscovite).
- 2.67 2.62. Chiefly quartz with minor plagioclase.
- 2.62 2.57. Quartz, K-feldspar, and plagioclase.
- 2.57 2.28. Microcline with minor quartz.
- <2.28. Microcline, some plagioclase (mostly weathered material), minor pyrite, and a trace of clinoptilolite.</p>
- -80 +120 (whole fraction). Quartz, plagioclase, K-feldspar with minor pyrite and marcasite.
- <u>-120 (whole fraction)</u>. Quartz with K-feldspar, plagioclase, marcasite, pyrite, and very minor clinoptilolite. Marcasite predominates over pyrite in the finest size material.

#### USBM-8

Similar to the preceding samples. There is noticeably less of the smoky quartz in this sample, however, and there is a bluish-green pigment in part of the clay matrix. An X-ray diffraction pattern of this material showed only montmorillonite and quartz and the nature of the pigment itself is still not known. It is a very minor constituent, but distinctive.

- -20 +40 mesh (whole fraction). Quartz, plagioclase, and K-feldspar (in about equal amounts and both fairly well weathered), minor pyrite, and clinoptilolite (with included pyrite).
- -40 +80 mesh (specific gravity fractions).
  - >3.31. Pyrite and marcasite. Very minor heavy minerals are sphene, garnet, zircon, and tourmaline.

- 3.31 2.85. Pyrite, marcasite, plagioclase (with pyrite), and quartz (with pyrite). Very minor heavy minerals are sphene, tourmaline, and garnet, and fluorapatite.
- 2.85 2.67. Quartz, plagioclase, minor muscovite, pyrite.
- 2.67 2.62. Quartz with subordinate plagioclase and very minor muscovite.
- 2.62 2.57. K-feldspar and quartz, minor plagioclase.
- 2.57 2.28. Microcline with very minor quartz and clinoptilolite.
- <2.28. Microcline, minor quartz, and clinoptilolite. The blue-green pigmenting material is concentrated in this fraction.</p>
- -80 +20 mesh (whole fraction). Quartz, plagioclase and K-feldspar, minor pyrite, and trace of clinoptilolite.
- -120 mesh (whole fraction). Same as above.

#### USBM-2a

Clay shale. Greenish-gray (5GY 6/1), silty, calcareous (calcite) clay transected by a thin (5 mm) pyritiferous calcareous (calcite) seam. The clay minerals are composed predominantly of Ca-montmorillonite with subordinate, and randomly interstratified, chlorite and illite (hydrous mica). The silt fraction is mostly quartz, microcline, pyrite, and minor albite. A very small amount of the quartz, pyrite, and microcline are also present in the clay-sized fraction. No clinoptilolite, nor marcasite were found in the sample.

## Chemistry of Formation Waters:

Figure 5 shows the location of wells studied. Some distant monitoring wells sampled to obtain a better understanding of the regional variations of the formation water chemistry are not shown. Prior to the introduction of lixiviant into the formation, a suite of samples was collected from the USBM test wells, a company production well, and two outlying company monitoring wells. Pumps were mounted in the wells and were used to obtain the water samples. The pumps all had been in place for several days before any samples were collected. Approximately five well volumes of water were pumped prior to the collection of any samples. The samples were all collected through a small bypass which diverted some of the flow from the well to a tee which allowed the water to be passed through a filter and/or a flow-through cell for measuring Eh and pH (fig. 6).

At each sampling of the well, a series of four samples were collected. The first sample was a 500-mL unfiltered, unacidified sample. Three 500-mL samples which had been filtered through a 0.1 µm membrane filter were then collected. One of the samples was acidified with 2 mL of analyzed 6 normal nitric acid. The other two samples were not acidified. One of the filtered samples was used for field analyses and the remaining three were kept for laboratory analyses. The samples were collected in polyethylene bottles and sealed with screw caps with a polyethylene cone fitting which provides an air-tight seal.

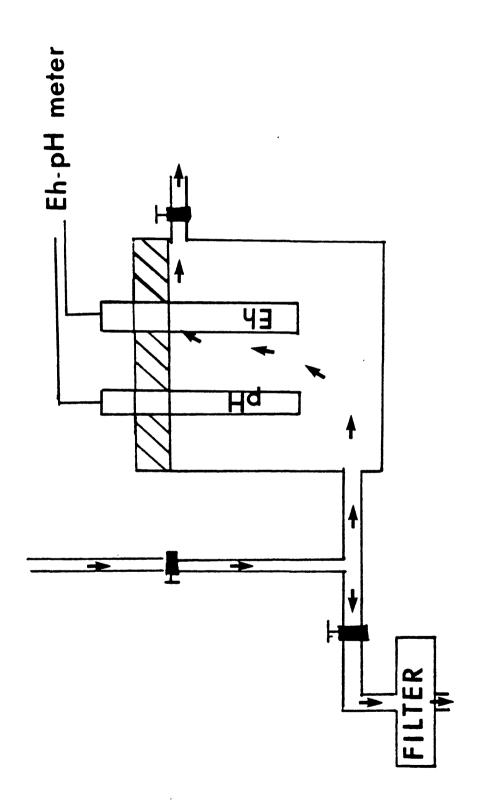


Figure 6. Schematic of the flow through cell used to obtain pH and Eh measurements as well as filtered samples.

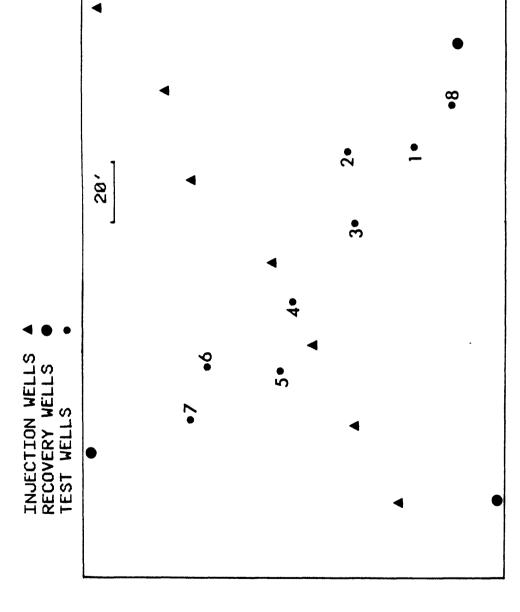


Figure 5. Location map for leaching experiment.

In addition to the pumped samples, formation waters were also obtained using a gas-tight downhole sampler that had been designed for sampling geothermal fluids. The downhole sampler would capture approximately 500-mL samples which then transferred through gas tight fittings into an evacuated (10<sup>-2</sup> torr) 500-mL glass bottle leaving a small (10 mL) headspace. The glass bottle was then sealed by means of 0-ring seals while still connected to the sampler. The samples were then retained for laboratory analyses of the dissolved gas contents of the water. In addition to the downhole water samples, a series of downhole temperature measurements were made using a maximum reading thermometer. The downhole temperature measurements were conducted at night while the air temperature was less than 15°C.

As the pumped samples were collected a series of field measurements were conducted to measure fluid properties and to obtain concentration data on fugitive constituents which could not be preserved by the sampling procedures (Eh, pH, and HCO<sub>3</sub>). Field analytical methods for constituents of interest to in-situ leach operations (Na, K, and Ca) were also tested.

The Eh and pH of the formation waters were measured simultaneously in a flow-through cell (fig. 6). A portion of the well flow that was diverted into the bypass tube was used to flush the plastic cell with four to five volumes of effluent (one cell volume is approximately 200 mL). The combination Eh and combination pH electrodes were then inserted into the plastic cell being careful to exclude air bubbles.

The flow through the plastic cell was reduced to approximately 20 mL/min. When the emf of the combination Eh electrode had stabilized (±10 mv), usually after 30 to 45 minutes, the Eh and pH values were recorded. In contrast to the Eh value, the pH value usually stabilized in a few minutes although continuous readings were taken until the Eh electrode values had stabilized. The temperature of the fluid in the cell was also measured with a mercury thermometer which had been previously calibrated against a platinum resistance thermometer. The combination Eh electrode was standardized with Zobell's solution and was found to be stable enough (±3 to 5 mv) that usually only one standardization per day was necessary. Before and after the pH measurements the pH electrode was standardized using pH 4, 7, and 9 buffers.

The bicarbonate concentration was determined in the field using the following titration procedure. A 100-mL aliquot of filtered formation water was placed into a beaker along with a magnetic stirring bar and 3 drops of methyl purple indicator. A combination pH electrode standardized using pH, 4, 7, and 9 buffers was transferred into the beaker. The solution was then titrated with standardized 0.05 normal sulfuric acid. Pairs of pH readings and acid volumes were recorded until the indicator turned gray at a pH of 5.1. A minimum of three pairs of acid volumes and pH values were then obtained between pH 5 and pH 4. The amount of bicarbonate was then computed from a least-squares regression of the entire titration curve which was used to calculate the end point exactly (Barnes, 1964). This method of

determining the end point is far more precise than the usual method of using a fixed end point of 4.5. The standardization of the combination pH electrode was again checked along with temperature at the conclusion of the titration. Any shifts were then used in the computation of the end point as required.

The increase in the Na and K concentrations of the lixiviant (usually formation water plus (NH<sub>4</sub>)<sub>2</sub>CO<sub>3</sub> with or without oxidant) during the leaching process are good indicators of the degree of ion-exchange occurring between the lixiviant and the formation. Hence a field analytic method for measuring Na and K concentrations in groundwater and lixiviant could prove to be a useful tool for on site monitoring of the performance of an in-situ leaching operation. Correspondingly, we tested the behavior of ion-selective electrodes specific for Na and K as possible field or on-stream analytical methods.

The K concentration was determined by taking a 100-mL aliquot of filtered formation water and adjusting the ionic strength by adding 2 mL of 6 molar NaCl solution. The K electrode and a double junction reference electrode were then immersed in the solution and the emf allowed to stabilize. The emf value was then recorded and the concentration determined from a calibration curve determined from a set of 3 to 4 standards. A similar procedure was followed for Na except that the ionic strength was adjusted with 3 mL of 4 molar KCl solution.

The Ca content of the formation water is of concern because of difficulties arising from precipitation of calcite during the leach operations. Radium and uranium co-precipitates with calcite resulting in a radioactive low level waste which must be disposed of. Calcium also interferes with the extraction of the uranium from the lixiviant. Hence, the ability to monitor Ca is of practical significance.

We tried two procedures as field analytical methods. The first was a standard titration with EDTA and the second was using a Ca ion-selective electrode. Due to difficulties with direct measurement, we had to use the electrode with an EDTA titration to improve the precision. However, it soon became apparent that the regular EDTA titration was far more reliable and use of the electrode was abandoned.

The three 500-mL samples which were taken back to the laboratory were analyzed by standard methods for the major constituents. Several methods were employed to check for trace element contents. One method was to evaporate to dryness 100 mL of sample and to do a quantitative analysis of the evaporate by emission spectroscopy. The second, more novel, method employed emission spectroscopy with an inductively coupled plasma. Table 2 shows which methods were employed to analyze which constituent.

Table 2. Methods employed for laboratory analyses of samples

Constit- uent	Atomic Absorp-	Spectro- photo- metric	Gravi- metric		Titra- tion	Plasma emission spectros- copy	Emission spectros- copy
SiO <sub>2</sub>	Х	x				X	х
Fe	X	X					X
Ca	X					X	X
Mg	X						X
Na	X						X
K	X	•					X
Li	X					X	X
Al	X					X	X
As							X
Ba							X
Cd							X
Cr							X
Cu							X
Рь							X
Mn							X
Hg							X
Мо							X
Se							X
Ag							X
Δ.							X
Zn							X
Ur		X				X	X
NH4				X			
SO <sub>4</sub>		X	X				
Cl				X	X		
F				X			
PO <sub>4</sub>		X					
В		X				X	X
H <sub>2</sub> S		X	X				
cō <sub>3</sub>		X	X		••		
нсб3					X		

The samples collected by the downhole gas-tight sampler were analyzed for the various gaseous components as follows. The major residual gases (gases in the headspace above the sample) were analyzed with a gas chromatograph equipped with a Carle Thermistor Detector and 6-foot Poropak Q and 20-foot molecular sieve 5A columns in series held at  $27^{\circ}\text{C}$ . Helium carrier gas at 60 psi inlet pressure was used for analysis of  $0_2$ , Ar,  $N_2$ , and  $\text{CH}_4$  while argon carrier gas at 50 psi inlet pressure was used for He and  $\text{H}_2$ . Hydrocarbon gases were analyzed with a Hewlett Packard flame ionization gas chromatograph. Dual 6-foot Poropak Q columns were used with helium carrier gas at an inlet pressure of 60 psi, and the analysis temperature programmed from  $30^{\circ}\text{C}$  to  $150^{\circ}\text{C}$ .

## Analytical Results:

The baseline data for the major constituents are summarized in table 3 while the analytical data for the dissolved gases are contained in table 4.

Well #602 was sampled and analyzed by the U.S. Geological Survey, the Texas Water Quality Board (TWQB), and the operating company. A detailed comparison of the three sets of analyses are listed in table 5. The data differ significantly only in uranium, the pH and HCO<sub>3</sub>. For pH and HCO<sub>3</sub> this is because our measurements were done in the field while the others were done on stored samples. CO<sub>2</sub> will escape from the stored samples, causing precipitation of calcite and thus lowering the HCO<sub>3</sub> content and increasing the pH. The filtered unacidified sample taken for laboratory analyses had a pH of 7.82 when measured in the laboratory three weeks later, compared to a field pH of 6.98.

Table 3. Baseline data for groundwater.
All values are in mg/L except for Eh (mv), pH and T°C.

	USBM 1	USBM 3	USBM 4	USBM 7	USBM 8	USBM 6#	Company #602
Eh	-131	-119	<b>-</b> 98	<b>-</b> 70	-140	<del>-</del> 85	-100
pН	6.90	7.01	6.97	7.18	6.95	7.11	6.98
Ť	24.5	24.5	25.4	24.8	25.4	24.5	25.4
Na	153	125	165	130	128	123	125.0
K	11.9	12.0	10.9	13.8	11.1	17	11.4
Ca	48.6	59.3	5 <b>7.</b> 5	57.0	53.0	56	55.0
Mg	5.4	5.9	5.8	5.1	5.7	5	5.8
Al	•003	.001	.003	.003	.003		.003
Fe	.12	.11	.12	.10	.11		.12
Li	•035	•035	.045	.040	.040		.04
SiO <sub>2</sub>	38	35	32	31	35		37.0
U	•01	.11	<b>.</b> 10	.09	.0006	-	.50
инз	•1	.1	.1	.1	.1		.1
S04	65	72	100	114	76		81.0
Cl	94	76	177	75	76		75.0
F	•55	.60	.50	•55	.60		<b>.</b> 55
PO <sub>4</sub>	.05	•05	.05	.05	•05		.05
HCO3	328	341	326	354	337		337
В	1.1	1.0	1.1	.8	1.23		1.2
As	-	-	-	-	-		.02
Cd	-	-	-	-	-		N.D.
Cu	-	-	-	-	-		.03
Pb	-	-	-	-	-		.03
Mn	-	-	-	-	-		.04
Mo	-	-	-	-	-		•50
V	-	-	-	-	-		.03
Zn	-	-	-	-	-		.03
Cr	-	-	-	-	-		N.D.
Hg	-	-	-	-	-		N.D.
Se	-	-	-	-	-		N.D.
Ag	-	-	-	-	-		N.D.

<sup>\*</sup> Field Analyses only

Table 4. Gas Analyses for downhole sampler.

Values reported as mg/L dissolved in water.

	USBM 1	USBM 3	usbm 7	Company 106	Company 115	usbm 3#
He	0.03	0.03	0.03	0.03	0.03	0.03
H <sub>2</sub>	.03	•03	.03	.03	•03	.03
Ar	.03	.056	.102	.125	1.804	.046
02	.03	.03	.03	.03	.03	.03
N <sub>2</sub>	26.44	3.684	3.978	6.481	57.21	3.581
СНц	•905	•915				
C2H6	.002	.002				
Propa	ne .002	.002				
NH3	.1	.1	. 1	.1	.1	high
H <sub>2</sub> Š	•2	•3	N.D.	N.D.	1.6	.2

<sup>\*</sup>Samples collected after the arrival of the lixiviant

The data in tables 3 and 4 were used to calculate mineral saturation through the use of the computer programs SOLMNEQ (Kharaka and Barnes, 1973) and WATEQ (Truesdell and Jones, 1974). The waters are in equilibrium with minerals of the host formation with but few exceptions. The most notable is pyrite, which is extremely supersaturated, with significant iron and hydrogen sulfide present in the formation water. The mineralogic evidence suggests that clinoptilolite is forming in the sands with pyrite but there are no thermodynamic data available to check this observation with the solution chemistry.

A most interesting result of the baseline study is the apparent indication that the orebody is currently forming. The strongest pieces of evidence are the strong Eh gradient across the deposit and the very rapid decrease in the uranium content of the water across the orebody. The pH of the formation waters showed no apparent correlation with the orebody; however, where data were available there was a strong correlation between calcite content of the well and the pH of the formation water removed from the well. The Eh gradient present in the orebody is apparently related to the migration of  $H_2S$ from deeper oil field brines which is subsequently oxidized to sulfate by the inflow of oxygenated groundwater. These phenomena are of significance to the in-situ leach operations. On the oxidizing side of the oxidation-reduction front uranium can be solubilized more readily with less or no additional oxidant, while on the reducing side significantly larger quantities of oxidant will be required to obtain the same uranium concentrations in solution.

Table 5. Comparison of Analyses for Baseline Data of Well #602 with those of the Texas Water Quality Board and the Operating Company

Element or Measurement	USGS	TWQB	Company
Eh (mv)	-100.0		
pH	6.93 0.3	8.1	7.3
ToC	25 <b>.</b> 4		
SiO <sub>2</sub> Fe	37 •12		
Ca	55	61	51
Mg	5 <b>.</b> 8	6.1	6
Na	125	120	135
K	11.4		
Li	.04	***	
Al	.003		
As	.02	.01	.02
Ba	.1	•5	•5
Cd	N.D.	.01	.002
Cr	N.D.	.01	.01
Cu	•03	.05	.02
Pb	•03	.05	.02
Mn	.04	.1	.06
Hg	N.D	.0005	.0001
Mo	.5	•5	•55
Se	N.D. N.D.	.002	.005 .002
Ag V	N.D. .02		.002
Zn	.03	.1	.03
U	.50	1.3	•53
NH <sub>3</sub>	.1	.1	.1
S0 <sub>4</sub>	81		72
Cl	75		78
F	•55		
PO <sub>4</sub>	.05		
В	1.20		.6
H <sub>2</sub> S	•30		
HCO <sub>3</sub>	337		280

#### LEACHING PHASE

## Lixiviant Chemistry Versus Time:

Methods used to sample the groundwater prior to the injection of the lixiviant were also employed to sample and preserve the lixiviant samples. The only difference in procedure was to cease field titrations for HCO<sub>3</sub> after the lixiviant had arrived and not to acidify the high carbonate samples with nitric acid. The analytical methods were all the same as used previously; however, the standards used in the analyses were made so as to have the same general matrix as the lixiviant.

The lixiviant was manufactured by dissolving gaseous ammonia and carbon dioxide in the groundwater. The lixiviant was put into the formation at the injection wells near USBM-4. The following wells were sampled daily or more frequently as conditions warranted: USBM-1, USBM-3, USBM-4, AND USBM-7. The data obtained are summarized in tables 6, 7, 8, and 9.

Table 6. Summary of Chemical Analyses for USBM-1

				2					•	,		•		
	9		9	11.2	166	12.8	41.5	5.10	;	;	1 0	;	75	0
۔ د	9-19	36.0	 	317	9	9.71	47.5	5.45	: :	: :	† .0°	69	8 8	<b>!</b>
• ~	3-23	26.0	7.20	308	148	11.6	51.0	5.64	;	;	<0.1	1	:	;
. ~	3-22	25.9	96.9	341	148	11.8	54.5	5.45	;	;	¢0.1	;	92	;
-	3-23	;	7.19	363	143	11.6	53.5	5.75	;	;	<b>*0.1</b>	;	;	;
9	3-25	28.0	B. 00	400	143	11.6	54.0	5.90	38	;	<b>60.1</b>	46	8	0.05
œ	3-28	28.0	7.50	392	140	11.7	24.0	5.85	38	;	<b>40.</b> 7	29	;	;
2	3-29	28.0	7.01	348	1 39	11.6	54.0	5.90	<b>4</b> 0	ł	<b>.0</b> ,	;	90	;
77	3-31	27.5	7.23	345	139	11.7	55.0	5.85	:	;	<b>40.1</b>	;	78	;
=	<del>7-</del> 5	;	7.44	367	138	11.6	91.5	<b>6</b> .00	36	;	<b>40.</b> 1	ł	;	;
51	<b>6-3</b>	26.0	1.75	363	137	11.6	26.0	6.10	i	;	<b>*0.1</b>	;	92	;
91	Į	26.0	7.17	358	136	11.9	54.0	5.95	;	;	<b>40.1</b>	99	;	;
11	4-5	24.0	7.50	!	135	;	;	5.90	ł	;	<b>*0.1</b>	ł	ł	9.0
97	9-4	24.5	7.31	334	139	11.5	76.3	6.05	;	;	<0.1	;	8	;
61	4-7	24.0	6.98	334	134	10	31.0	7.00	36	;	<0.1	99	;	;
20	9-	24.0	96.9	7	126	70	30.6	7.20	ł	;	<b>40.</b> 3	;	85	;
22	4-10	24.0	6.77	479	164	12	30.6	9.20	:	ł	<0.1	;	16	1
23	<b>4-1</b>	24.0	9.05	: ;	126	37	18.8	17.8	9	900	510	3	1	5.0
3 2	: -	20.00		;	1.20	144	5	24.2	: ;	1680	953	: ;	;	19.5
. 40	4-12	9.00			: :	318	2	26.4	;	2760	1566	;	112	; ;
,		9 0	900	: :	194	36.2	: -	22.8	;	4980	7697	1	} ;	;
3 2	77-7			<b>!</b>		3 5	:		35	65.40	27.7	: ;		
2 5		9 0			674	9 7	: -		; ;	6480	9636	a	133	,
<b>.</b> 6		9 6	***	)		900	•			9		•	90.	: 1
•		0.00		i	5	616	7.		; ;	0000	2756	1 6		
<b>=</b> :	61-4	28.0	97.5	!	1	283	7:	26.1	<b>X</b> :	0995	BEEF.	2	77	c. <del>1</del>
F :	4-21	28.0	3.	;	1 38	191	9.	10.3	33	7,60	1266	1	911	* :
32	4-23	28.0	9.00	!	102	116	3.8	8.8	;	1320	749	1	110	18.5
9	4-24	28.0	9.58	;	167	197	1.2	29.5	23	2640	1498	;	;	۰ ک
37	4-25	28.2	9.28	;	<b>58</b> 8	270	1.2	29.4	18	4020	2822	:	121	3.3
8	4-26	29.0	9.49	ŀ	126	;	1.0	30.4	<b>1</b> 6	6780	3849	;	127	× 52
39	4-27	30.0	9.30	;	148	;	5.6	32.4	01	8461	4802	29	139	5.8
<b>9</b> :	4-28	30.0	<b>6</b>	;	;	187	9.7	20.4	ŀ	7201	4087	;	734	;
<b>‡</b> :	4-29	30.0	9.23	;	: 1	011	5.6	14.5	;	4740	7690	;	77	1 :
7	4-30	29.2	90.6	;	211	78	3.0	5.01	ł	3780	2145	;	;	0.5
42.5	4-30	29.5	9.30	;	116	63	2.5	11.4	;	4 380	2486	98	;	;
Ţ:	-s	29.0	9.50	ł	273	7	2.3	12.5	;	4980	2827	;	120	;
£3.5	-	30.0	9.60	;	282	2	2.3	13.0	;	5340	3031	;	;	;
=	2-5	29.0	9.71	;	283	92	2.2	11.8	=	2460	3099	;	:	1.7
44.5	2-5	30.0	9.30	;	270	83	1.9	11.11	;	2400	3065	114	;	!
<b>‡</b> 2	5-3	29.0	9.50	;	294	88	2.3	10.7	;	5280	2997	;	126	;
45.5	5-3	29.5	;	;	134	88	2.1	9.01	;	5220	2963	;	!	!
46	5-4	29.0	9.50	:	147	96	2.4	10.4	;	4980	2827	ŀ	;	;
46.5	<b>7-</b> 5	29.5	9.50	;	134	67	2.3	12.1	;	4860	2759	146	;	1
47	5-5	29.0	9.30	:	148	83	2.8	11.2	12	5220	2963	;	122	1.0
47.5	5-5	29.5	9.40	;	278	65	7	11.7	<b>:</b>	5160	2929	:	<b>:</b>	; ;
48	9-9	30.0	9.30	;	267	26	2.3	12.9	;	5160	2929	;	;	;
20	9-9	30.0	9.50	;	233	120	2.4	14.4	;	5520	3133	167	123	;
51	6-5	29.5	9.40	;	130	121		14.7	;	5220	2963	: :	<u> </u>	1
51.5	9-1	0 00	9	1	280	127	,		;	240	3065	107		
22	5-10	29.0	50	1	133	336	: -		12	55.80	2900	: ;	:	: 1
52.5	5-10	29.0	08.30	;	278	95.1			: :	5580	1167	וניכ	;	;
53	2-5	29.0	9.50	;	282	147		14.2	Œ	55.20	31 33	: ;	122	¦
53	5-12	29.0	9.40	ł	290	160	2.3	15.7	١ :	5200	3235	;	; ;	;
53.5	5-12	29.0	9.40	;	288	167	1.7	15.4	Œ	5820	3304	;	;	1
3	5-13	0.60	05.6	ŀ	282	172	7	14.6	١ ;	0009	3406	223	¦	;
55	5-14	: :	: :		233	2	: ;		:	} :	;	:	;	0.7
8	5-15	ł	ł	;	227	120	8	9.00	;	4620	2622	114	120	1
57	5-16	!	;	;	: :	117	7	11.3	ł	4680	2656	:	<b>!</b>	1
58														
	7-6	;	:	;	;	2	ر د	۲ ،		ABOO	2726	787	;	;

	61-6	:	1.10	313	120	13.7	65.5	9.6	\$	:	40.1	;	96	0.11
	1-31	;	7.03	199	120	12.4	57.0	5.7	;		*0°	<b>;</b>	1 7	;
	3-23	36.0	9R.9	ī	00.1	12.0	32.5	6.3	;		40.1	1 ;	*	;
	3-25	28.0	6.85	7	129	11.6	59.c	9. B.	2	:	40.1	17	3	:
	3-28	26.0	7.10	- ?	129	11.3	58.0	\$. 6.	;	1	<b>4</b> 0.	:	2	:
	3-59	27.5	7.03	356	130	11.3	28.0	<b>9</b> .0	35	;	<b>1</b> .0	:	:	:
	1-31	27.5	7.30	747	200	11.6	5 <b>6</b> .0	•. o	;	:	40.1	09	2	:
	1-1	36.0	7.39	916	101	12.2	59.5	6.2	;		<b>.</b> 0.	;	:	:
	4-7	26.0	7.43	163	147	12.8	o. 3	7.0	35		40.1	;	\$	:
		2 10	**	;	376	1.38	1.0	12.2	or C		1022	9	;	:
				;	346	305	-	5.11	50		1737	:	77	:
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	ĵ.	o. •	-	:	707		•					1 3	:	;
	9-	24.0	17.6	:	787	2	•	ć .	: :		1166	6	2 :	ł
	1-1	24.5	<b>9.</b>	:	212	252	•	=======================================	2		4292	2	=	:
		25.0	11.6	:	237	193	•	21.3	:		4326	;	;	:
	6-7	25.0	3.5	;	345	197	0.3	17.3	:		2372	:	126	:
	4-10	25.0	9.47	:	287	180	•	19.1	<b>98</b>		2895	:	;	:
				;	91.0	010	•	22.0	36		31 34	11	123	5.0
	***			ì				9	2		7	: }	2	
	71-1	73.0	CT .	:	י י	707					****			;
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	91-1	29.0	9.43	:	972	332	٥.٢	87.8	=		2484	;	145	2.7
	4-17	29.0	0M.6	:	247	344	<b>.</b>	23.6	:		2552	9 3	743	2.5
	717	2		;	220	2110	•	11.11	70		24.20	;	:	٠.٠
					:	Ş		4 41	3 -		4126	-	\$1.1	•
	17-	2	2 .	1	: :				:		32.5	:	:	:
	-77	28.0	7.7	:	7		:		; ;			; ;	1	•
	1-74	33.0	<b>8</b> .42	;	197	ŝ	•	0.01	=		777	;	:	;
	4-25	28.0	8.55	:	338	126	<b>.</b>	10.2	;		9218	:	:	:
	4-26	28.0	97.6	;	243	137	3.3	21.12	13		1260	;	113	0.
	4-27	28.0	9.50	;	;	390	7.7	43.0	;		1942	:	611	o. S
	4-28	20.00	30	;	223	16.3	7.7	29.6	;		3747	67	139	:
	- 30		,	;	771	946			;		2998	1	126	3.0
	9-7-9	. 4		;	**	16.3		15.2	=		2078	;	117	1.9
				;					: 1		20.01	;		; <b>:</b>
	7-	6.6	7 .	:		•	•		}		95.75	4	; ;	1
_	2-1	30.0	9.71	:	2	80	7.		;		• (0)	8	;	1
	2-5	29.5	8.01 10.01	:	335	=	3.5	17.4	=		2453	:	:	:
	;	:	:	;	197	:	₹.	16.0	:		1022	:	1	1 ;
	2-5	29.5	9.30	;	273	113	9.e	18.3	:		2725	:	171	 
		:	:	;	276	3	7.7	11.1	;		:	;	;	:
	(-)	20.0	•	;	26.7	101	2.0	18.9	70		3888	901	126	:
			:		3,4			9 91	; ;		2024	:	:	:
•	7.	:	: ;	:	6 6		•		}		9010	i		;
	<b>1</b> -5	29.0	ų.	;	757	3	•	•	:		2007	1 5	1	; ;
<u>د</u>	7-5	29.5	ø. 8	:	762	2	7.7	17.6	:		193	101	171	-
	5-5	29.0	7.	:	257	22	o. 7	0.91	:		3416	:	:	:
	9-6	29.0	9.5	:	270	7	7.5	15.8	:		2929	:	:	₹.
	(-)	20.0	•	:	262	72	9.0	15.9	;		2827	;	122	:
						: 6		4	91		2461	717	:	;
,		6.67		;		2 :	:		:			:		1
•	3-5	29.5	٥.	:	726	3		7:	:		267	;	:	1
	<b>8-8</b>	29.5	9.S	:	238	01	5.2	13.7	:		3000	:	: ;	:
•	6-6	28.5	9.4	:	238	011	5.2	===	:		3066	ž	137	:
	5-10	26.5	7.6	;	238	105	2.3	13.2	:		2963	;	;	:
		9		;	265	801	2.4	13.4	:		2998	;	;	;
		. 40		: :	25.2	1	7	•	:		3100	:	;	:
	77-0		,	1							901	7	;	:
•	2-17	28.5	¥.	:	657	57	•		;		200		1 2	
	5-13	28.5	7.6	:	32B	132	•	2.5	•		97.76	;	Ç	•
	:	:	:	:	255	156	7.7	15.1	:		3372	:	:	:
:	:	:	;	:	212	140	7.6	6.91	;		2929	:	:	:
	:	:	:	;	213	134	3.5	11.3	;	1794	2623	129	;	:
	: :		: ;	;			•	4	:		2623	:	17.	:
	1													
	}	:	:				•					:	:	

Table 8. Summary of Chemical Analyses for USBM-4

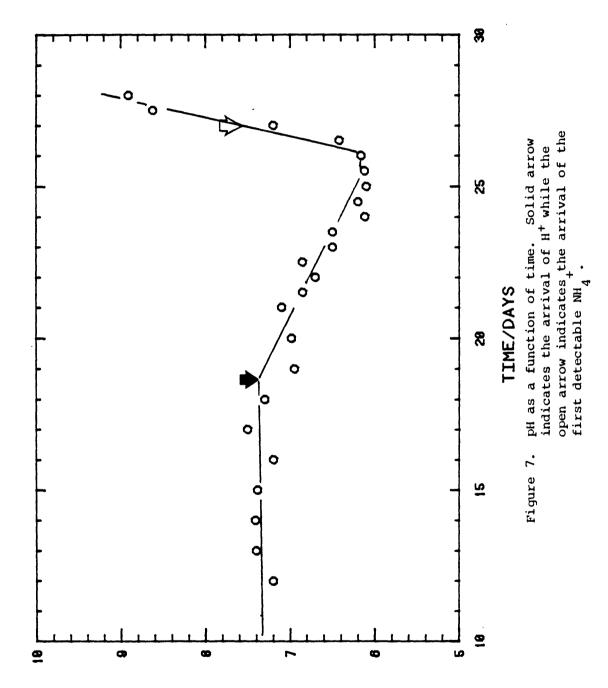
8         1         1-20          6.97         326         166         10.8         73         12         32          40.1           13         2         3-21         26.5         7.18         306         165         10.9         73.5         12          40.1           2         3-21         26.5         7.18         306         165         10.7         51         6          40.0           3         4.23         26.0         7.40         347         116         25.0         26         6          40.0           3.9         6.5         3.25         2.6         3.6         4.0          140         25.0         26         6          40.0         27.0         4.0         4.0          140         25.0         26         1.0         4.0          4.0         1.0         4.0          4.0          4.0          4.0         2.0         9.0         9.0         9.0         9.0         9.0         9.0         9.0         9.0         9.0         9.0         9.0         9.0         9.0         9.0 <th></th> <th>Day</th> <th>Date</th> <th><math>T^{\bullet}C</math></th> <th><b>3.</b></th> <th>H∞³-</th> <th>Мà</th> <th>¥</th> <th>င်ဒ</th> <th>Mg</th> <th>sio<sub>2</sub></th> <th>co<sup>3</sup>2-</th> <th>HN 4</th> <th>so 4-</th> <th>ಶ</th> <th><b>5</b></th>		Day	Date	$T^{\bullet}C$	<b>3.</b>	H∞³-	Мà	¥	င်ဒ	Mg	sio <sub>2</sub>	co <sup>3</sup> 2-	HN 4	so 4-	ಶ	<b>5</b>
2         3-21         26.5         7.18         308         165         10.9         72.5         112		-	3-20	1	6.97	326	166	10.8	7.3	12	32	;	<0.1	ł	177	0.1
3         3-22         24.3         6.90         377         128         12.4         57         6		~	3-21	26.5	7.18	308	165	10.9	72.5	12	i	!	<0.1	100	:	;
4         1-23         26.0         7.40         341         116         10.7         51         7          480           6.5         1-25         26.0         7.40         341         116         56.0         36         14         34         14         480           6.5         1-26         1-26         1-26         12         36         14         34         372           9         1-28          8.40          181         56.0         36         18         372           11         3-10         2.88         9.30          255         273         2.6         26         26         19         372           11         4-2          2.0         9.30          200         174         1.8         29          1860           15         4-2          2.0         9.30          200         174         1.8         29          1860           15         4-2          2.0         174         1.8         29          1860           16         4-3         3.0		۳	3-22	24.3	06.9	377	128	12.4	23	9	!	1	<0.1	;	1	{
6         13-25         28         8.40          140         25.0         26         6          408           9         1-25         1-25         1-26         26         26         26         26         24         34         3720           9         1-28          9.80          252         260         2.6         27         20 <td></td> <td><b>~</b></td> <td>3-23</td> <td>26.0</td> <td>7.40</td> <td>341</td> <td>136</td> <td>10.7</td> <td>51</td> <td>7</td> <td>!</td> <td>1</td> <td>40.1</td> <td>;</td> <td>:</td> <td>;</td>		<b>~</b>	3-23	26.0	7.40	341	136	10.7	51	7	!	1	40.1	;	:	;
6.5         13-25          9.80          181         56.0         36         14         34         3720           9         3-28          6.40           178         2.6         25         19         194         34         3720           10         3-28          6.40          252         260         2.5         19         19         244         34         3721           11         3-28          6.00          252         265         173         26         25         19         26         19         304         10         20         10		9	3-25	28	8.40	;	140	25.0	<b>5</b> 6	9	!	480	272	1	:	;
9         3-28          6+40           138         2.6         25         19         1074           11         3-29          6+30          252         260         2.5         19         21         2241           11         3-30         28.8         9,30          252         260         2.5         19         21         2241           12         4-3         28.6         9,30          200         174         1.8         29          1002           15         4-3         28.6         9,30          200         174         1.8         29          1002           15         4-4         30.0         9,35          107         103         20          1050           18         4-6         30.0         9,35          107         105          1050           19         4-7         20.0         177         105         10         1050          1050           10         4-8         20.0         9,35          107         1050		6.5	3-25	ł	9.80	;	181	56.0	36	14	34	3720	2111	ł	1	s
10         3-29          6.90          255         260         2.5         19         21         9241           11         3-30          26.8         9.30          221         203         2.0         26          1002           13         4-1         26.9         9.30          205         177         1.8         20         14         19603           14         4-2           200         174         1.8         20         14         19603           15         4-3         30.0         9.30          100         174         1.8         20          19603           16         4-4         30.0         9.30          181         127         1.6         1.7         11602           17         4-6         20.0         10.05          195         56         2.3         1.7         11602           20         4-7         28.0         9.64          199         2.5         19         2.7         19           21         4-13         31.0         9.64 </td <td></td> <td>6</td> <td>3-28</td> <td>ł</td> <td>8.40</td> <td>1</td> <td>!</td> <td>378</td> <td>5.6</td> <td>25</td> <td>19</td> <td>10741</td> <td>6097</td> <td>1</td> <td>146</td> <td>09</td>		6	3-28	ł	8.40	1	!	378	5.6	25	19	10741	6097	1	146	09
11         3-10         28.8         9.30          255         273         4.3         28         18         1752           12         4-31         26.0         9.38          221         203         1.0         26.0         1.0 </td <td></td> <td>10</td> <td>3-29</td> <td>;</td> <td>B.90</td> <td>;</td> <td>252</td> <td>260</td> <td>2.5</td> <td>61</td> <td>21</td> <td>9241</td> <td>5245</td> <td>93</td> <td>144</td> <td>901</td>		10	3-29	;	B.90	;	252	260	2.5	61	21	9241	5245	93	144	901
12         4-31         26.0         9.38          221         203         1.0         26          1002           13         4-1         26.5           200         177         1.8         20         14         1903           14         4-2             200         177         1.8         20         14         1903           15         4-3         10.0         9.30          177         130         6.5         30          15722           16         4-6         20.0         9.30          177         130         6.5         30          15922           17         4-6         20.0         9.30          177         130         6.5         19         7         1603           19         4-7         28.0         9.37          193         37         2.3         12.2         1041           20         4-9         28.0         9.6          193         37         2.3         1041           21         4-1         27.0         9.68		11	3-30	28.8	9.30	;	255	273	4.3	28	18	17522	9946	!	1	150.5
13         4-1         28.5         9.50          205         177         1.8         20         14         19803           14         4-2            170         174         1.8         20         14         19803           15         4-3         30.0         9.30          177         130         6.5         30          156         80          156         180          156         80          156         180          156         180          156         180          156         180          156         180          156         180          156         180         173         173          180         180         2.3         17.1          180           10         4-8         27.0         9.68          180         36         2.3         17.1          180           20         4-8         27.0         9.68          180         3.7         2.3         17.1          104           21		12	4-31	26.0	9.38	;	221	203	2.0	<b>36</b>	1	13022	7391	;	154	143
14         4-2            200         174         1.8         29          18602           15         4-3         30.0         9.30          177         130         6.5         30          1872           17         4-5         30.0         9.35          177         105         7.5         30          10501           17         4-5         30.0         9.35          177         105         7.5         30          10501           19         4-6         28.0         10.05          156         89         2.5         19         7         9481           21         4-9         28.0         9.82          193         37         2.3         17.1          10401           21         4-9         28.0         9.64          193         37         2.3         17.1          1041           22         4-11         27.0         9.64          194         44         3.5         8.3          1041           28         4-13		13	4-1	28.5	9.50	;	205	177	1.8	20	14	19803	11240	!	1	;
15         4-3         30.0         9.30          177         130         6.5         30         7         15722           16         4-4         30.0         9.30          177         130         6.5         30         7         1582           17         4-5         30.0         9.30          181         127         7.5         30          13082           18         4-6         28.0         9.78          195         56         2.3         12.2          9481           20         4-9         28.0         9.78          195         56         2.3         12.2          1041           21         4-9         28.0         9.64          180         33         2.3         17.1          1041           22         4-10         27.0         9.64          180         33         2.2         7.2         1041           24         4-11         31.0         9.47          177         35         3.2         3.2         3.2         3.2         3.2           28         4-18<		7	4-2	;	;	;	200	174	1.8	29	;	18602	10559	!	1	;
16         4-4         30.0         9.30          181         127         4.3         27          1362           17         4-5         30.0         9.35          177         105         7.5         30          1050           19         4-6         28.0         9.78          195         56         2.3         12.2          1651           20         4-8         27.0         9.97          195         56         2.3         17.1          1041           21         4-9         28.0         9.68          193         37         7.4          1041           24         4-10         27.0         9.64          180         3.7         7.4          1041           24         4-11         27.0         9.64          180         3.7         7.4          1041           26         4-13         31.0         9.41          184         3.5         8.6         10         1021           28         4-15         31.0         9.41          1		15	<b>4-3</b>	30.0	9.30	;	177	130	6.5	30	7	15722	8924	;	180	127.5
17         4-5         30.0         9.35          177         105         7.5         30          10501           18         4-6         28.0         10.05          168         89         2.5         19         7         9481           20         4-8         27.0         9.78          195         56         2.3         17.1          1041           21         4-9         28.0         9.68          193         37         2.3         8.3         6         961           22         4-10         27.0         9.68          180         34         2.2         7.4          1041           24         4-11         27.0         9.64          180         3.7         7.4          1041           26         4-13         31.0         9.47          194         44         3.5         7.2         7.2         7.2         1021           28         4-18         31.0         9.47          179         29         3.3         3.4         1021           31         4-21         29.0		16	4-4	30.0	9.30	;	181	127	4.3	27	!	13682	1766	100	158	150.1
18         4-6         28.0         10.05          168         89         2.5         19         7         9481           19         4-7         28.0         9.78          195         56         2.3         12.2          8681           20         4-8         27.0         9.97          193         37         7.4          1041           21         4-9         28.0         9.68          180         35         2.3         17.1          1041           22         4-10         27.0         9.68          180         3.7         7.4          1041           24         4-11         27.0         9.68          180         3.7         7.4          1041           26         4-13         31.0         9.64          194         44         3.5         8.6         10.01         10.01           28         4-13         31.0         9.41          194         44         3.5         8.6         11         10.01           39         4-21         29.0         8.81		17	4-5	30.0	9.35	;	177	105	7.5	30	1	10501	2960	!	145	170.6
19         4-7         28.0         9.78          195         56         2.3         12.2          6581           20         4-8         27.0         9.97          193         37         2.3         17.1          1044           21         4-9         27.0         9.68          180         36         3.7         7.4          1041           24         4-11         27.0         9.68          180         35         3.7         7.4          1041           26         4-13         31.0         9.59          194         44         3.5         8.6         10         1021           26         4-15         31.0         9.41          194         44         3.5         8.6         10         1021           28         4-16         31.0         9.41          177         35         3.4         6.5         11         10021           34         4-21         29.0         9.41          173         29         3.4         6.5         11         10021           35         4-		18	9-4	28.0	10.05	;	168	68	2.5	61	7	9481	5381	133	140	160.3
20         4-8         27.0         9.97          219         69         2.3         17.1          10141           21         4-9         28.0         9.68          193         37         2.3         8.3         6         961           24         4-10         27.0         9.68          180         35         7.4          1031           26         4-13         31.0         9.64          194         44         3.5         8.6         10         1021           26         4-13         31.0         9.47          177         35         8.6         10         1021           28         4-15         31.0         9.41          179         29         3.3         5.4         12         9901           34         4-28         29.0          179         29         3.3         5.4         12         9901           34         4-21         29.0         9.2          130         18         11.2         3.4         10.0           34         4-22         29.2          130         18 </td <td></td> <td>19</td> <td>4-7</td> <td>28.0</td> <td>9.78</td> <td>;</td> <td>195</td> <td><b>2</b>6</td> <td>2.3</td> <td>12.2</td> <td>;</td> <td>8581</td> <td>4870</td> <td>!</td> <td>131</td> <td>167.8</td>		19	4-7	28.0	9.78	;	195	<b>2</b> 6	2.3	12.2	;	8581	4870	!	131	167.8
21         4-9         28.0         9.82          193         37         2.3         8.3         6         9961           22         4-10         27.0         9.68          180         36         3.7         7.4          10381           24         4-11         27.0         9.64          180         3.7         7.2          10381           26         4-13         31.0         9.59          194         44         3.5         8.6         10         10261           28         4-15         31.0         9.41          179         29         3.4         6.5         11         10261           34         4-21         29.0         8.83          131         19         6.7         5.7         34         600           36         4-21         29.0         8.83          130         18         31.2         5.1         12.9         38         1080           36         4-21         29.5          130         18         11.2         991           37         4-24         28.5         8.58		20	<b>4</b> -8	27.0	9.97	:	219	68	2.3	17.1	;	10141	5756	!	!	139.5
22         4-10         27.0         9.68          180         36         3.7         7.4          10381           24         4-11         27.0         9.64          180         33         2.2         7.2          10621           26         4-13         31.0         9.59          194         44         3.5         8.6         10         10621           28         4-15         31.0         9.47          177         35         3.4         6.5         11         10021           31         4-18         31.0         9.41          179         29         3.3         5.4         12         9901           34         4-21         29.0         8.83          143         22         5.1         12.9         38         1080           36         4-24         28.5         8.58          130         18         31.2         25.1         12.9         38         1080           39         4-26         28.5         8.48          130         18         10.0         40.0         40.0           41		21	6-9	28.0	9.83	;	193	37	2.3	8.3	9	1966	5654	1	143	;
24         4-11         27.0         9.64          180         33         2.2         7.2          10621           26         4-13         31.0         9.59          194         44         3.5         8.6         10         10261           28         4-15         31.0         9.47          177         35         3.4         6.5         11         10261           31         4-18         31.0         9.41          179         29         3.3         5.4         12         9901           34         4-21         29.0         9.41          139         6.7         5.7         34         600           36         4-21         28.5         9.2          143         22         5.1         12.9         38         1080           39         4-26         28.5         8.58          130         19         8.1         9.3          683           39         4-26         28.3         8.48          142         19         26.9         13.2         3.6         4.0           40         4-26 <t< td=""><td></td><td>22</td><td>4-10</td><td>27.0</td><td>89.6</td><td>;</td><td>180</td><td>36</td><td>3.7</td><td>7.4</td><td>;</td><td>10391</td><td>5892</td><td>129</td><td>144</td><td>;</td></t<>		22	4-10	27.0	89.6	;	180	36	3.7	7.4	;	10391	5892	129	144	;
26         4-13         31.0         9.59          194         44         3.5         8.6         10         10261           28         4-15         31.0         9.47          177         35         3.4         6.5         11         10021           31         4-18         31.0         9.41          179         29         3.3         5.4         12         9901           34         4-21         29.0         8.83          131         19         6.7         5.7         34         600           36         4-24         28.5         9.2          143         22         5.1         12.9         38         1080           39         4-26         28.5         8.58          130         18         31.2          683           39         4-26         28.3         8.48          142         19         26.9         13.2         480           40         4-26         29         7.49         342         119         16         9.6          482           41         4-26         29         7.25         3		<b>74</b>	4-11	27.0	9.64	;	180	33	2.2	7.2	;	10621	6009	;	138	S
28         4-15         31.0         9.47          177         35         3.4         6.5         11         10021           31         4-18         31.0         9.41          179         29         3.3         5.4         12         9901           34         4-28         29.0         8.83          131         19         6.7         5.7         34         600           36         4-24         28.5         9.2          143         22         5.1         12.9         38         1080           38         4-24         28.5         8.58          130         18         31.2         12.5          683           39         4-26         28.3         8.48          142         19         26.9         13.2         36         660           40         4-26         28.3         8.32          142         19         26.9         13.2         36         10.0         40           41         4-28         29         7.49         342         119         16         63.0         10.0         40          482	۰	<b>3</b> 6	4-13	31.0	9.59	;	194	44	3.5	9.6	01	10261	5824	!	;	;
31         4-18         31.0         9.41          179         29         3.3         5.4         12         9901           34         4-21         29.0         8.83          131         19         6.7         5.7         34         600           36         4-24         28.5         9.2          143         22         5.1         12.9         38         1080           37         4-24         28.5         8.58          130         18         31.2         12.5          683           39         4-26         28.3         8.48          130         19         26.9         13.2         36         660           40         4-27         28.5         8.32          142         19         26.9         13.2         38         480           41         4-28         29         7.49         342         119         16         30.0         10.0         40           42         4-29         28         7.25         342         119         16         30.7         10.3         36            43         4-30         2	_	28	4-15	31.0	9.47	;	177	35	3.4	6.9	11	10051	5688	;	!	;
34         4-21         29.0         8.83          131         19         6.7         5.7         34         600           36         4-23         28.5         9.2          143         22         5.1         12.9         38         1080           37         4-24         28.5         8.58          130         19         12.5          683           38         4-26         28.3         8.48          130         19         26.9         13.2         38         480           40         4-27         28.5         8.32          118         19         26.0         9.6          480           41         4-29         29         7.49         342         119         16         53.0         10.0         40            42         4-29         28         7.25         342         119         16         30.7         10.3         36            43         4-30         28         7.29         320         141         18         30.0         11.6         36            49         5-6         28 <td>~</td> <td>31</td> <td>4-18</td> <td>31.0</td> <td>9.41</td> <td>;</td> <td>179</td> <td>29</td> <td>3.3</td> <td>5.4</td> <td>12</td> <td>1066</td> <td>5620</td> <td>9</td> <td>148</td> <td>ł</td>	~	31	4-18	31.0	9.41	;	179	29	3.3	5.4	12	1066	5620	9	148	ł
36         4-23         28.5         9.2          143         22         5.1         12.9         38         1080           37         4-24         28.5         8.58          130         18         31.2         12.5          683           38         4-25          9.33          130         19         8.1         9.3         36         660           40         4-26         28.3         8.48          118         19         26.9         13.2         38         480           41         4-26         28.5         8.32          118         19         26.0         9.6          482           41         4-26         29         7.49         342         119         16         63.0         10.0         40          482           42         4-28         28         7.69         320         125         18         30.7         10.3         36          49           43         4-30         28         7.20         320         141         18         30.0         11.6         36 <td>_</td> <td>ž</td> <td>4-21</td> <td>29.0</td> <td>8.83</td> <td>;</td> <td>131</td> <td>19</td> <td>6.7</td> <td>5.7</td> <td>34</td> <td>009</td> <td>340</td> <td>!</td> <td>100</td> <td>;</td>	_	ž	4-21	29.0	8.83	;	131	19	6.7	5.7	34	009	340	!	100	;
37         4-24         28.5         8.58          130         18         31.2         12.5          683           38         4-25          9.33          130         19         8.1         9.3         36         660           39         4-26         28.3         8.48          142         19         26.9         13.2         38         480           40         4-27         28.5         8.32          118         19         26.0         9.6          482           41         4-28         29         7.49         342         119         18         63.0         10.0         32          482           42         4-30         28         7.69         320         125         18         30.2         10.0         40            43         5-6         28         7.20         320         141         18         30.0         11.6         36	_	36	4-23	28.5	9.5	;	143	22	5.1	12.9	38	1080	613	!	106	S
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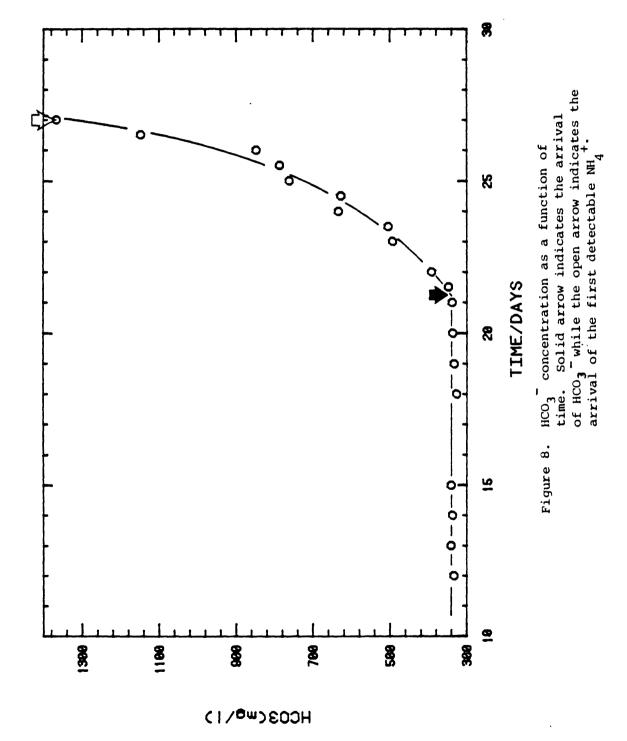
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Initially the water arriving at the wells was displaced formation water. If the flow is slug flow as assumed by various hydrologic models used for modelling (Shock, 1977) then one would expect to see an increase in pH,  $NH_{H}$  concentration and  $CO_{2}$  concentration as the lixiviant arrives at the well. Slug flow would result in all of the ions arriving more or less at the same time. If the diffusion rate of an ionic species is greater than the flow rate, the ionic species could arrive early. However, because of the relatively slow diffusions rates of most ions, this is unlikely. In addition, if an ionic species is specifically adsorbed on the surface of the mineral grains, it will be retarded in its arrival with respect to an ionic species which does not adsorb on surfaces. Specific adsorption would allow for a chromatographic separation of ions in the moving lixiviant and invalidate assumptions regarding slug flow. The phenomenon of ions being separated or arriving at different times was indeed observed, particularly in USBM-7 which had the longest arrival time for the fluid. Figures 7, 8, 9, 10, and 11 illustrate the various arrival times of the moving lixiviant as indicated by changes in various chemical parameters. Based on these data, it would appear that migration rates decrease in the order H > HCO $_3$  > Mg > Cl > Na > $K > Ca > NH_{h}$ , or that the relative adsorption of the ions increases in the same order.





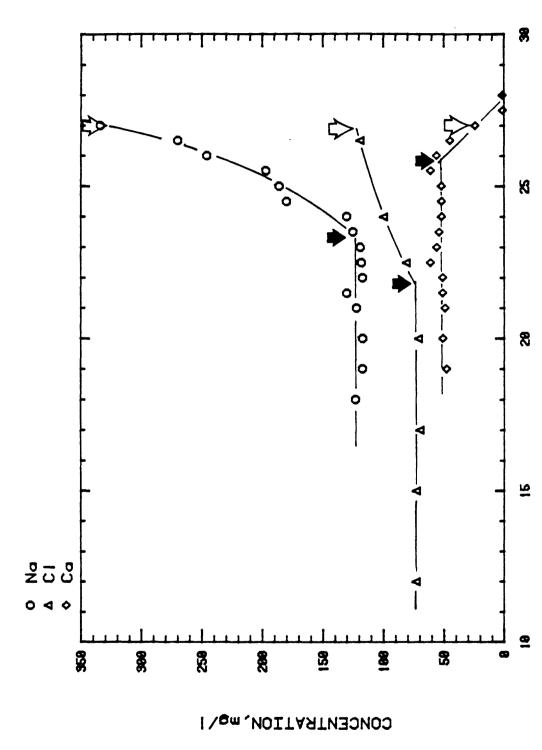
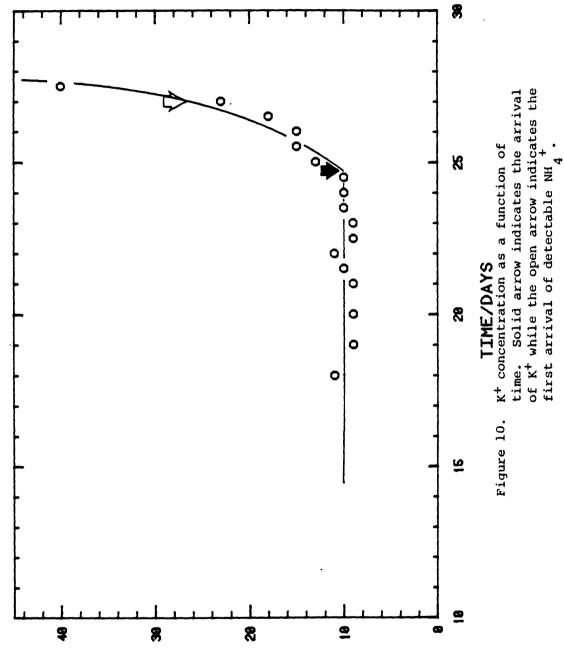


Figure 9. Na<sup>+</sup>, Cl<sup>-</sup>, and Ca<sup>++</sup> concentration as a function of time. Solid arrows indicate the arrivals of Na<sup>+</sup>, Cl<sup>-</sup> and Ca<sup>++</sup> while the open arrow indicates the arrival of the first detectable NH<sub>4</sub>.

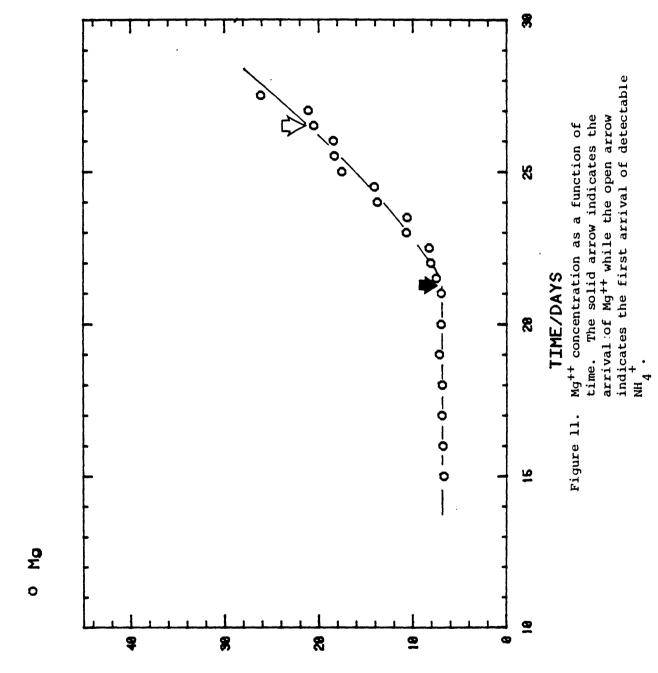
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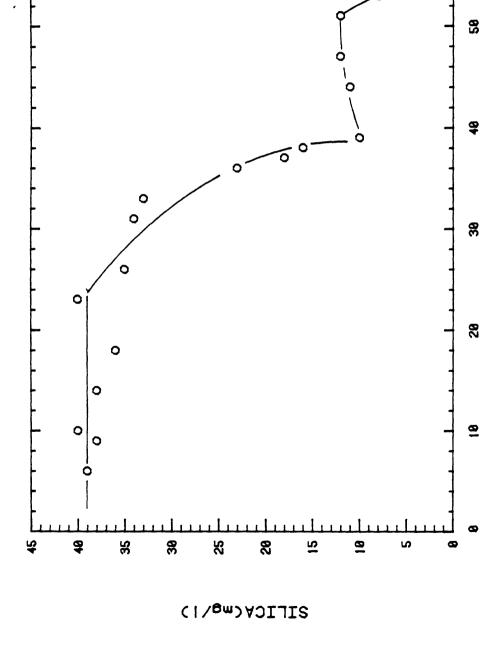


Figure 12. The SiO<sub>2</sub> concentration as a function of time for USBM-1, illustrating the unexpected decrease in silica concentration.

Several other interesting phenomena occurred with respect to changes in the concentration of various elements during the leaching phase. The lixiviant with only air as an oxidant successfully mobilized uranium near the injection points which were in the oxidized zone. However, as these solutions moved outward, the uranium content decreased significantly. This phenomenon would be expected in the reduced region of the ore deposit, but was unexpected in the oxidized portion. There are several possible explanations for the behavior of uranium in USBM-7:

- l. Uranium migration is slower than that of the other elements (except  $NH_{ij}$ ). The direction of the flow in the field was reversed on 4/19 and the maximum uranium concentration may not have been achieved.
- 2. Slower migration of uranium indicates its selective adsorption on clays and zeolites. Significant adsorption and/or ion exchange may have occurred, thus reducing the uranium concentration.

Using SOLMNEQ and WATEQ, saturation with various silicate phases was again calculated using an average groundwater composition plus the appropriate concentration of ammonium carbonate. On the basis of these calculations one would predict that the concentration of silica would remain unchanged or increase slightly since the stability of most of the silicate phases had decreased. As can be seen in figure 12, the response was just the opposite of what was expected: the silica concentration showed a marked decrease. Only in one well,

USBM-4, did the silica ever regain its former concentration; this was however, associated with the reversal in the flow direction and the subsequent hydrologic isolation of USBM-4. The decrease can seemingly only be related to the formation of a silicate phase not contained in the computer codes such as buddingtonite (NH<sub>1</sub> feldspar) or some similarly related form. The reaction of the ammonium carbonate plus silica with the clays could yield the ammonium feldspars plus hydrogen ion which could explain the source of the early arriving hydrogen ion detected in the various wells.

The Na, K, and Mg concentrations are more strongly controlled by ion exchange reactions than by chemical equilibria involving dissolution and precipitation except possibly for some contribution from the reaction of montmorillonites with the lixiviant to form ammonium feldspars. The concentration of all three elements increases in the lixiviant in such a way as to suggest a preferential release of Mg >K > Na, although due to the observed chromatographic effects this preferential or kinetic exchange reaction can not be confirmed without laboratory experiments designed to separate kinetic from chromatographic effects.

The behavior of Ca at first glance is somewhat predictable; i. e., as the CO<sub>3</sub> content increases the Ca concentration decreases.

However the decrease in Ca is not as rapid as would be expected and the resulting concentrations appear to be in approximate equilibrium, slightly supersaturated or in a few cases extremely supersaturated

with respect to calcite. These observations appear to indicate that either the kinetics of CaCO<sub>3</sub> precipitation are responsible for the slow decline or Ca is being added by ion exchange at or near the same rate as the precipitation of CaCO<sub>3</sub>. The behavior of Cl during the leaching operation is an almost perfect example of homogenization of a chemical gradient. The make up water had a slightly higher Cl concentration than USBM-1, USBM-3, and USBM-7 and a lower concentration than USBM-4. With time all four wells approached a uniform value, except for USBM-7 which showed fluctuations due to the reversal of flow in the field.

The  $SO_{ij}$  concentration shows a progressive increase with time in all wells. The largest increase was noted in USBM-1 after the reversal of flow in the field and after  $H_2O_2$  had been injected into the formation. These increases are due to the oxidation of pyrite by the oxidant. A concomitant increase in Fe concentration was not detected; however, at these high pH values one would expect the Fe to precipitate as amorphous iron oxi-hydroxide, and thus not be detected at the observation wells.

During the course of the leach operation there were no statistically significant variations of the concentrations of Al, Li, F, or B. This may be partially due to analytical problems for Al, Li, and F which were near their detection limits. The B concentration most likely indicates that it behaves as a conservative element throughout the leaching processes.

Although prior to the arrival of the lixiviant, the Eh electrode produced reasonably stable values; after the arrival of the lixiviant the readings became erratic. This behavior may have been related to the large increase in ionic strength of the fluids or because of fouling of the platinum electrode by the ammonia solution and/or fine suspended precipitates (gels) such as iron oxi-hydroxides, clays, etc. In conjunction with the problems related to the Eh electrode, an extremely high failure rate was observed for pH electrodes after the lixiviant began arriving. The cause for the electrode failures appeared to be clogging of the frit with fine grained particulates, which might also relate to the failures of the Eh combination electrodes as well.

During the course of the leaching of the orebody, the temperature of the lixiviant being produced from the sampling well systematically increased with time. The temperatures were initially about  $25^{\circ}\text{C}$  and slowly drifted up to around  $31^{\circ}\text{C}$ . This phenomena is of a greater magnitude than would be expected from chemical dissolution and precipitation reactions. The dissolution of  $(NH_4)_2\text{CO}_3$  in water is endothermic which produces an opposite temperature change than was noted.

## Comparison of Field Versus Laboratory Analyses:

The field determination of pH and  $\ensuremath{\text{HCO}_{2}}$  are the most accurate methods for determining these quantities, since they are interdependent and cannot be preserved. Proper preservation methods exist for Na, K, and Ca; hence, if any field analytical method for these constituents is to be of any practical use, it must be capable of accurately reproducing the real values for the concentration. Figures 13, 14, and 15 illustrate the field data plotted versus the laboratory values for Na, Ca, and K respectively, for samples where the lixiviant had yet to arrive. The analyses done by field titration with EDTA for Ca appear to be the best with 56% of the measured values within ±10% of the atomic adsorption spectroscopy (AAS) values and with 74% of the measured values within ±20% of the AAS values. next most reliable set of field analyses were the Na+ analyses done by ion-selective electrode. For Na, 51% of the analyses lie within ±10% of the AAS values while 84% of the values lie within ±20% of the AAS values. The worst field method appears to be the K analyses done by ion-selective electrode. Only 39% of the field measured values lie within ±10% of the AAS values and only 59% lie within ±20% of the AAS values.

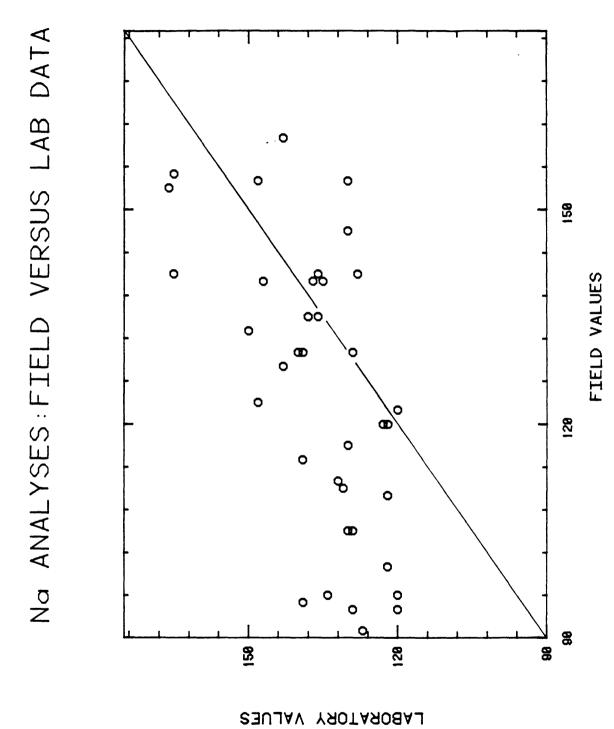
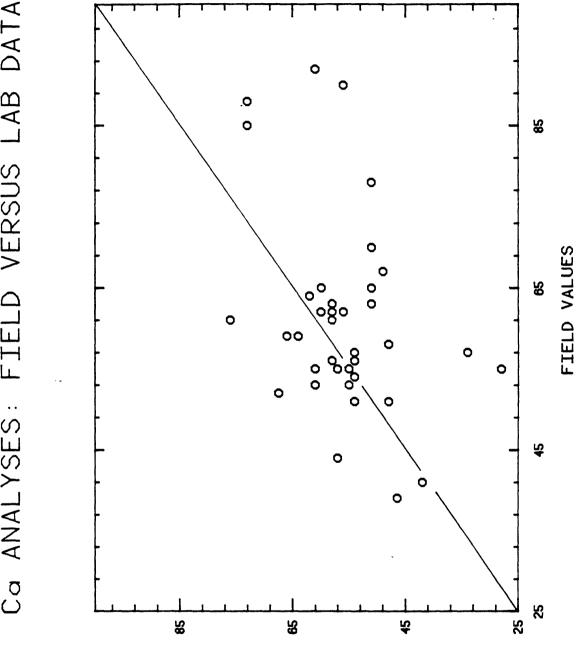


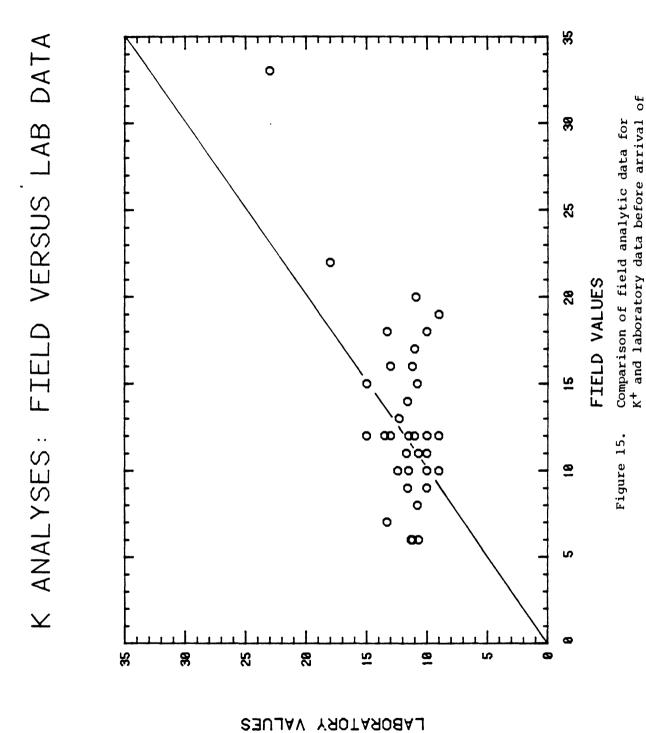
Figure 13. Comparison of field analytic data with laboratory data before arrival of lixiviant.





Comparison of field analytic data with laboratory data before arrival of lixiviant. Figure 14.

LABORATORY VALUES



lixiviant.

51

After the arrival of the NH<sub>\(\pmu\)</sub> the reliability of the field analytical data dramatically decreased except for the K analyses which actually improved. The Ca analyses, which had been the best, suddenly became the worst with discrepancies commonly of an order of magnitude. This probably relates to the increasing concentration of Mg as well as the dissolution of fine grained (<0.1 micron) CaCO<sub>3</sub> by the EDTA as the values measured in the field are uniformly too high. The reliability of the Na electrode decreased markedly with only 45% of the measured values being within ±20% of the AAS values. The K electrode, however, improved its reliability slightly with 65% of the field measured values being within ±20% of AAS values. There appears to be no rational explanation for this behavior of the K electrode except that perhaps the field measured values are fortuitously closer to the real concentration.

In general, the results of the field analytical data for Na, K, and Ca are not encouraging. The data at best are only qualitative, particularly after the lixiviant arrives. The behavior of the Na electrode can be improved by the addition of  $NH_{ll}$  to the standards but the results do not warrant the extra effort. In contrast, the field pH and  $HCO_3$  measurements are very reliable and could be employed with monitor wells to detect an excursion many days prior to  $NH_{ll}$  reaching the monitor well; thus allowing for the early corrective action to be taken.

## CONCLUSIONS

This report presents data on the chemical changes occurring during the in-situ leaching of an uranium orebody which has been well characterized mineralogically prior to leaching. These data hence constitute a data set against which any models for describing the leaching of an uranium orebody may be tested for reliability. These data also suggest areas which warrant further study:

(a) characterization of the chromatographic separation of ions,

- (b) kinetics of the ion-exchange of the clay minerals, (c) the influence of zeolites on exchange and chromatographic behavior of ions (d) the ion-exchange capacity of zeolites and clays for unanium
- ions, (d) the ion-exchange capacity of zeolites and clays for uranium, (e) the kinetics and thermodynamics of the oxidation of uranium minerals by various oxidants, and (f) studies centered on the methodology for extracting the NH<sub>11</sub> which has been ion exchanged and/or reacted with the host formation. The later area of research would require as a companion to detailed laboratory work, a comprehensive study of the restoration to initial baseline conditions of a leached uranium orebody similar to the study summarized in this report. In light of the complexities encountered during the leaching of this orebody, similar studies of other types of orebodies should be conducted for both the alkaline and acid leaching systems.

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